

## Lattice Boltzmann Method

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## Introduction & History

Let's get to know LBM



#### Introduction

- Two extreme scales for modeling fluid flow (Mele 2013)
  - Macro-Scale
    - Uses PDE Equations such as Navier Stokes equation
    - Normally solved numerically using FDM, FEM, or FVM
  - Micro-Scale
    - Models individual molecules
    - Behavior governed by Hamilton's equation
    - There are too many molecules to practically model virtually anything useful



#### Introduction

- LBM splits the gap between these two scales
  - Considers a collection of molecules as a unit
  - Able to accurately model macro-scale behavior by considering average behavior of these collections of molecules
  - Behavior governed by Boltzmann equation



Molecular dynamics Hamilton's equation

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#### Introduction

- Advantages
  - LBM solved locally so it is easy to break the problem into calculations that can be done in parallel by multiple computer processers (Mele 2013).
  - Meshing is quasi-instantaneous and computationally simple
- Disadvantages
  - Difficult to simulate scenarios with a high Mach numbers
  - Thermo-hydrodynamic scheme is absent



- Boltzmann Equation (1800's)
  - Developed by Ludwig Boltzmann
  - Describes the dynamics of an ideal gas
  - The Lattice Boltzmann Equation, which governs behavior in the LBM, is a discretized form of the Boltzmann Equation





- Lattice Gas Automata
  - Precursor to LBM
  - Developed by Hardy, Pomeau, and de Pazzis in the 1970's
  - Initially was widely praised as a revolutionary technique.
  - Featured on front page of Washington Post on November 19, 1985
  - Problems with LGA led to the need for the development of LBM





- Lattice Gas Automata
  - Disadvantages
    - Statistical noise
    - Needs to simulate a large number of particles in order to reach an acceptable solution
    - Computationally inefficient due to its discrete state calculations





- Lattice Boltzmann Method
  - Developed incrementally in the 1980's
  - Overcomes statistical noise associated with LGA by replacing boolean particle occupation variables with single particle distribution functions
  - Distribution functions are an averaged quantity, so there is no need to average the state of a large quantity of cells to define macroscopic behavior







# General Principle

Essence of Lattice Boltzmann Method



### **General Principles**

- LGA (Lattice Gas Automata)
- Lattice Boltzmann Equation
- Collision and Streaming Stages
- LBM vs. CFD (Computational Fluid Dynamics)
- Validation of LBM

### Lattice Gas Automata (LGA)



- Originated from early 1990's.
- Lattice Automaton used to simulate fluid flows
- Comprises of a lattice with different states on sites.
- Lattice Gas: states are represented by particles with certain velocities.
- State at each site is purely boolean: there either *is* or *is not* a particle travel in each direction.
- Evolution is done by two steps in each time step: streaming and collision
- Precursor to Lattice Boltzmann Method

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### Microscopic Dynamics

Microscopic particles inside fluids

## Fictitious particles moving along lattice links





#### Lattice Gas Automata (LGA)



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### Lattice Gas Automata (LGA)



FHP model First introduced in 1986 by Frisch, Hasslacher and Pomeau • Consider a set of boolean variables:

$$n_i(x,t), \quad i=0,1,\ldots M$$

- Particle presentation
  - $n_i(x,t) = 0$  No particles at site x and time t  $n_i(x,t) = 1$  A particle is present at site x and time t
- Collision rules

$$\Omega_i(n(x,t)) = -1, 0, 1$$

Mass conservationMomentum conservation

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LGA 
$$n_i(x+e_i\delta t,t+\delta t) = n_i(x,t) + \Omega_i(n(x,t))$$

#### **Probability distribution function**

$$f_i = f_i(x, \xi, t)$$

**LBM**  $f_i(x+e_i\delta t,t+\delta t) = f_i(x,t) + \Omega_i(f(x,t))$ 

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### **Macroscopic** Properties

#### **Probability distribution function**



Flow properties easily computed from particle distribution values per time step

$$\rho = \sum_{i} f_{i} \qquad u = \frac{\sum_{i} f_{i} e_{i}}{\rho} \qquad v = \frac{2\tau - 1}{6}$$

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#### Streaming on Lattice

#### **A D2Q9 Lattice Model**





Image from Indo-German winter academy 2011

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#### **Collision Computation**

Bhatnagar-Gross-Krook (BGK) collision operator for equilibrium

$$\Omega_i = -\tau^{-1} \left( f_i(x,t) - f_i^{EQ}(\rho,u) \right)$$

where,  $\boldsymbol{\tau}$  is the relaxation time

$$f_i^{EQ}(\rho, u) = \rho(A + B(e_i \cdot u) + Cu^2 + D(e_i \cdot u)^2)$$

where, -A, B, C, D are constants defined by lattice geometry

### **Boundary Handling**

Microscopic Numerical Fluid Solver

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### Algorithm of LBM



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#### LBM vs. CFD

#### **Conventional CFD Method**

#### **Construction of fluid equations**

*Navier-Stokes equation* 2<sup>nd</sup>-order PDE, nonlinear convective term

**Discrete approximation of PDE** Finite difference, finite element, etc

#### **Numerical integration**

Solve the equations on a given mesh and apply PDE boundary conditions

#### **Lattice Boltzmann Method**

**Discrete formulation of kinetic theory** *Lattice Boltzmann equation* 1st-order PDE, simple advection

**No further approximation** The equations are already in discrete form

**Numerical integration** Solve on lattices and apply kinetic based BC

**Simple conversion to fluid variables** These are theoretically shown to obey the required fluid equations



Navier-Stokes equation for incompressible flow

 $\mu \frac{\partial^2 u}{\partial x^2} = \frac{\partial p}{\partial y}$ 

Available exact analytical solution

$$u(x) = \frac{\Delta P}{2\mu L} x(x - H)$$



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#### Analytical Fluid Parabolic Velocity Profile





#### Validation of the LBM





• We can solve varies Fluid Dynamics problems with LBM

Image from nus.edu & combustion fundamental group



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# Governing Equation of LBM

Manipulation & Interpretation



We start from general Boltzmann Equation

$$\frac{\partial f}{\partial t} + \frac{p}{m} \cdot \nabla f + F \cdot \frac{\partial f}{\partial p} = \left(\frac{\partial f}{\partial t}\right)_{coll} - - -(1)$$

In which:

- f is a particle distribution function
- F is external force field acting on the particle
- m is particle mass
- p is particle momentum
- t is time



To derive LB equation, assume zero force field Also note that momentum over mass is particle velocity

Together with (1) yields:

$$\frac{\partial f}{\partial t} + \vec{\xi} \cdot \nabla f = \left(\frac{\partial f}{\partial t}\right)_{coll} - -(2)$$

In which:

•  $\xi$  is microscopic velocity  $\frac{p}{\xi} = \xi$ 



Collision term is usually approximated using Bhatnagar-Gross-Krook (BGK) collision operator

$$\Omega_i = -\tau^{-1} \left( n_i - n_i^{EQ} \right)$$

In which:

- $\Omega$  is the collision term
- $\tau$  or  $\lambda$  is a relaxation time representing the amount of time it consumed to return to equilibrium state.
- n or f is the particle distribution function
- n<sup>EQ</sup> or g is the distribution function in equilibrium state.





Assemble BGK collision term with LHS yields the general Lattice Boltzmann Equation:



in which:

- f is the single particle distribution function.
- $\xi$  is the microscopic velocity vector
- $\lambda$  is the relaxation time due to collision
- g is the Boltzmann-Maxwellian distribution function.

$$g \equiv \frac{\rho}{\left(2\pi RT\right)^{D/2}} \exp\left(-\frac{\left(\xi - u\right)^2}{2RT}\right)$$

in which:

- D is the dimension of space
- R is the ideal gas contant
- ρ, T and u are the macroscopic density of mass, temperature and velocity respectively. They are moments of distribution function f.



Compute macroscopic quantities (moments of distribution function f)

$$\rho = \int f d\xi = \int g d\xi$$
  

$$\rho u = \int \xi f d\xi = \int \xi g d\xi$$
  

$$\rho \varepsilon = \frac{1}{2} \int (\xi - u)^2 f d\xi = \frac{1}{2} \int (\xi - u)^2 g d\xi$$

Macroscopic quantities can be represented by integrating the distribution function in proper order

#### That's the beauty of LBM



#### Discretized LB Equation

Chapman-Enkog assumption

$$\int h(\xi) f(x,\xi,t) d\xi = \int h(\xi) g(x,\xi,t) d\xi$$
$$h(\xi) = A + B \cdot \xi + C\xi \cdot \xi$$

in which:

• A and C are arbitrary constants, B is an arbitrary constant vector

By writing LB equation in an ODE form and implementing Chapman-Enkog assumption

#### We can discretize LB equation in time

$$\frac{df}{dt} + \frac{1}{\lambda}f = \frac{1}{\lambda}g$$
$$\frac{d}{dt} \equiv \frac{\partial}{\partial t} + \xi \cdot \nabla$$

The Equation can be formally integrated over time step  $\delta_t$ 



#### Discretized LB Equation

$$f(\mathbf{x} + \boldsymbol{\xi} \delta_t, \boldsymbol{\xi}, t + \delta_t) = \frac{1}{\lambda} e^{-\delta_t/\lambda} \int_0^{\delta_t} e^{t'/\lambda} g(\mathbf{x} + \boldsymbol{\xi} t', \boldsymbol{\xi}, t + t') dt' + e^{-\delta_t/\lambda} f(\mathbf{x}, \boldsymbol{\xi}, t).$$

Assuming that  $\delta_t$  is small enough and g is smooth enough locally, the following approximation can be made:

$$g(\mathbf{x} + \boldsymbol{\xi}t', \boldsymbol{\xi}, t + t') = \left(1 - \frac{t'}{\delta_t}\right) g(\mathbf{x}, \boldsymbol{\xi}, t)$$
  
+  $\frac{t'}{\delta_t} g(\mathbf{x} + \boldsymbol{\xi}\delta_t, \boldsymbol{\xi}, t + \delta_t)$   
+  $O(\delta_t^2), \quad 0 \leq t' \leq \delta_t.$ 

The leading terms neglected in the above approximation are of the order of  $O(\delta_t^2)$ . With this approximation, Eq. (8) becomes

$$\begin{aligned} f(\mathbf{x} + \boldsymbol{\xi} \delta_t, \boldsymbol{\xi}, t + \delta_t) &- f(\mathbf{x}, \boldsymbol{\xi}, t) \\ &= (e^{-\delta_t / \lambda} - 1) [f(\mathbf{x}, \boldsymbol{\xi}, t) - g(\mathbf{x}, \boldsymbol{\xi}, t)] \\ &+ \left( 1 + \frac{\lambda}{\delta_t} \left( e^{-\delta_t / \lambda} - 1 \right) \right) \\ &\times [g(\mathbf{x} + \boldsymbol{\xi} \delta_t, \boldsymbol{\xi}, t + \delta_t) - g(\mathbf{x}, \boldsymbol{\xi}, t)]. \end{aligned}$$

If we expand  $e^{-\delta_t/\lambda}$  in its Taylor expansion and, further, neglect the terms of order  $O(\delta_t^2)$  or smaller on the right-hand side of Eq. (10), then Eq. (10) becomes

$$f(\mathbf{x} + \boldsymbol{\xi} \boldsymbol{\delta}_t, \boldsymbol{\xi}, t + \boldsymbol{\delta}_t) - f(\mathbf{x}, \boldsymbol{\xi}, t) = -\frac{1}{\tau} [f(\mathbf{x}, \boldsymbol{\xi}, t) - g(\mathbf{x}, \boldsymbol{\xi}, t)],$$

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#### Discretized LB Equation

Recall: we can calculate macroscopic quantities by integrating in momentum space.

## The integration can be approximated by quadrature up to a certain degree of accuracy.



#### Discretized LB Equation

The approximating quadrature takes the form:

$$\int \psi(\xi) g(x,\xi,t) d\xi = \sum_{\alpha} W_{\alpha} \psi(\xi_{\alpha}) g(x,\xi_{\alpha},t)$$

Where  $\Psi(\xi)$  is a polynomial of  $\xi$ , W $\alpha$  is the weight coefficient of the quadrature, and  $\xi \alpha$  is the discrete velocity set. Accordingly, the hydrodynamic moments can be computed by:

$$\rho = \sum_{\alpha} f_{\alpha} = \sum_{\alpha} g_{\alpha}$$

$$\rho u = \sum_{\alpha} \xi_{\alpha} f_{\alpha} = \sum_{\alpha} \xi_{\alpha} g_{\alpha}$$

$$\rho \varepsilon = \frac{1}{2} \sum_{\alpha} (\xi_{\alpha} - u)^{2} f_{\alpha} = \frac{1}{2} \sum_{\alpha} (\xi_{\alpha} - u)^{2} g_{\alpha}$$

Where:

$$f_{\alpha} \equiv f_{\alpha}(x,t) \equiv W_{\alpha}f(x,\xi_{\alpha},t)$$
$$g_{\alpha} \equiv g_{\alpha}(x,t) \equiv W_{\alpha}g(x,\xi_{\alpha},t)$$

**Question becomes finding:** 

- **1. A approximation of distribution** function f
- 2. Weight coefficients


### Approximation of Distribution Function

Recall Boltzmann-Maxwellian distribution function:

$$f \equiv \frac{\rho}{\left(2\pi RT\right)^{D/2}} \exp\left(-\frac{\left(\xi - u\right)^2}{2RT}\right)$$

Assume D=2, which means a 2-D case



$$f_{\alpha} = \rho w_{\alpha} \left[ 1 + \frac{\xi \cdot u}{RT} - \frac{u \cdot u}{2RT} + \frac{(\xi \cdot u)^2}{2(RT)^2} \right]$$
$$f_{\alpha}^{EQ} = \rho w_{\alpha} \left[ 1 + \frac{\xi \cdot u'}{RT} - \frac{u' \cdot u'}{2RT} + \frac{(\xi \cdot u')^2}{2(RT)^2} \right]$$

 $RT = c_s^2 = c^2/3$  Cs is the sound speed of the system



### Weighting Coefficients

Weight  $W\alpha$  depends on Lattice arrangements



$$w_{\alpha} = \begin{cases} \frac{4}{9}, & \alpha = 9\\ \frac{1}{9}, & \alpha = 1, 2, 3, 4\\ \frac{1}{36}, & \alpha = 5, 6, 7, 8 \end{cases}$$

#### Lattice Boltzmann Method





D3Q19 Lattice model Image from ASME Digital Collection

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#### Summary





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## Calculation Example

Steady Channel Flow



#### Problem Description

- D2Q9 model
- 2 by 2 system, 4 lattices
- Channel flow from left to right
- Boundary condition--bounce back
- Initial parameter

$$\rho = 1.0$$

$$\tau = 1.0$$

$$du = 1 \times 10^{-7}$$







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For each lattice in D2Q9 model, we present velocity by combination of 9 matrices, each matrix contains distribution function f $\alpha$ ,  $\alpha$ =1,2,...,9



Assume a initial state:

$$f1 = f2 = \ldots = f9$$

$$f_{\alpha} = \rho / 9, \alpha = 1, 2, 3..., 9$$

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#### Hand Calculation Example









**Distribution Function** 

$$(f1) = \begin{pmatrix} \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \end{pmatrix} (f2) = \begin{pmatrix} \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \end{pmatrix} (f3) = \begin{pmatrix} \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \end{pmatrix}$$
$$(f4) = \begin{pmatrix} \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \end{pmatrix} (f5) = \begin{pmatrix} \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \end{pmatrix} (f6) = \begin{pmatrix} \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \end{pmatrix}$$
$$(f7) = \begin{pmatrix} \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \end{pmatrix} (f8) = \begin{pmatrix} \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \end{pmatrix} (f9) = \begin{pmatrix} \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9} & \frac{1}{9} \end{pmatrix}$$

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$$(f1 \rightarrow) \left( \begin{array}{c} \frac{1}{9} & \frac{1}{9} \\ \frac{1}{9}$$



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Calculate Macroscopic Quantities



$$\rho = \begin{pmatrix} 1 & 1 \\ 1 & 1 \end{pmatrix} \qquad \begin{array}{c} U_x(1) + du \\ U_x(3) + du \end{array}$$

$$U_x = \begin{pmatrix} 0 & 0 \\ 0 & 0 \end{pmatrix} \qquad \begin{array}{c} U_x(1) + du \\ U_x(1) + du \end{pmatrix}$$

$$U_{x} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} \qquad U_{y} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$$
$$U \swarrow = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} \qquad U \swarrow = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$$
$$U \swarrow = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} \qquad U \searrow = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$$



Calculate Macroscopic Velocities

 $\rho_{\alpha} = \sum_{\alpha} f_{\alpha} = \frac{1}{9} \times 9 = 1$  $U_{x} = \frac{1}{9} ((f1 + f5 + f6) - (f3 + f7 + f8))$  $U_{y} = \frac{1}{2} \left( (f6 + f2 + f7) - (f5 + f4 + f8) \right)$  $U = U_{x}^{2} + U_{y}^{2}$  $U \nearrow = U_x + U_y$  $U \searrow = U_x - U_y$  $U \wedge = -U \wedge$  $U \swarrow = -U \nearrow$ 

 $U_x(1) + du$  $\rho = \begin{pmatrix} 1 & 1 \\ 1 & 1 \end{pmatrix} \qquad U_x(1) + du \\
U_x(3) + du \\
U_x = \begin{pmatrix} 1e - 7 & 0 \\ 1e - 7 & 0 \end{pmatrix} \qquad U_y = \begin{pmatrix} 0 & 0 \\ 0 & 0 \end{pmatrix}$  $U = \left( \begin{array}{cc} 1e - 7 & 0 \\ 1e - 7 & 0 \end{array} \right)$  $U \nearrow = \begin{pmatrix} 1e-7 & 0 \\ 1e-7 & 0 \end{pmatrix} \quad U \swarrow = \begin{pmatrix} -1e-7 & 0 \\ -1e-7 & 0 \end{pmatrix}$  $U \searrow = \begin{pmatrix} -1e-7 & 0 \\ -1e-7 & 0 \end{pmatrix} \quad U \searrow = \begin{pmatrix} 1e-7 & 0 \\ 1e-7 & 0 \end{pmatrix}$ 

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Calculate Equilibrium State Distribution Function

$$f_{\alpha}^{EQ} = \rho w_{\alpha} \left[ 1 + \frac{\xi \cdot u'}{RT} - \frac{u' \cdot u'}{2RT} + \frac{(\xi \cdot u')^{2}}{2(RT)^{2}} \right]$$

$$f_{\alpha}^{EQ} = \rho w_{\alpha} \left[ 1 + \frac{\xi \cdot u'}{RT} - \frac{u' \cdot u'}{2RT} + \frac{(\xi \cdot u')^{2}}{2(RT)^{2}} \right]$$

$$f_{\alpha}^{EQ} = \rho w_{\alpha} \left[ 1 + \frac{\psi \cdot u'}{RT} - \frac{\psi \cdot u'}{2(RT)^{2}} + \frac{(\xi \cdot u')^{2}}{2(RT)^{2}} \right]$$

$$f_{\alpha}^{EQ} = \rho w_{\alpha} \left[ 1 + \frac{\psi \cdot u'}{RT} - \frac{\psi \cdot u'}{2RT} + \frac{(\xi \cdot u')^{2}}{2(RT)^{2}} \right]$$

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$$f_{\alpha}^{EQ} = \rho w_{\alpha} \left[ 1 + \frac{\psi \cdot u'}{RT} - \frac{\psi \cdot u'}{2RT} + \frac{(\psi \cdot u')^{2}}{2(RT)^{2}} \right]$$

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$$f_{\alpha}^{EQ} = \rho w_{\alpha} \left[ 1 + \frac{\psi \cdot u'}{RT} - \frac{\psi \cdot u'}{2RT} + \frac{(\psi \cdot u')^{2}}{2(RT)^{2}} \right]$$

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$$f_{\alpha}^{EQ} = \rho w_{\alpha} \left[ 1 + \frac{\psi \cdot u'}{RT} - \frac{\psi \cdot u'}{2RT} + \frac{(\psi \cdot u')^{2}}{2(RT)^{2}} \right]$$

$$f_{\alpha}^{EQ} = \rho w_{\alpha} \left[ 1 + \frac{\psi \cdot u'}{RT} - \frac{\psi \cdot u'}{2RT} + \frac{(\psi \cdot u')^{2}}{2(RT)^{2}} \right]$$

$$f_{\alpha}^{EQ} = \rho w_{\alpha} \left[ 1 + \frac{\psi \cdot u'}{RT} - \frac{\psi \cdot u'}{2RT} + \frac{(\psi \cdot u')^{2}}{2(RT)^{2}} \right]$$



Calculated Equilibrium State Distribution Function

$$\begin{pmatrix} f1^{EQ} \rightarrow \end{pmatrix} = \begin{pmatrix} 0.01234568 & 0.012345679 \\ 0.01234568 & 0.012345679 \end{pmatrix} \begin{pmatrix} f2^{EQ} \uparrow \end{pmatrix} = \begin{pmatrix} 0.012345679 & 0.012345679 \\ 0.012345679 & 0.012345679 \end{pmatrix} \begin{pmatrix} f3^{EQ} \leftarrow \end{pmatrix} = \begin{pmatrix} 0.01234567 & 0.012345679 \\ 0.01234567 & 0.012345679 \end{pmatrix} \begin{pmatrix} f3^{EQ} \leftarrow \end{pmatrix} = \begin{pmatrix} 0.01234567 & 0.012345679 \\ 0.01234567 & 0.012345679 \end{pmatrix} \begin{pmatrix} f3^{EQ} \leftarrow \end{pmatrix} = \begin{pmatrix} 0.003086 & 0.003086 \\ 0.003086 & 0.003086 \end{pmatrix} \begin{pmatrix} f6^{EQ} \checkmark \end{pmatrix} = \begin{pmatrix} 0.003086 & 0.003086 \\ 0.003086 & 0.003086 \end{pmatrix} \begin{pmatrix} f6^{EQ} \checkmark \end{pmatrix} = \begin{pmatrix} 0.003086 & 0.003086 \\ 0.003086 & 0.003086 \end{pmatrix} \begin{pmatrix} f6^{EQ} \checkmark \end{pmatrix} = \begin{pmatrix} 0.003086 & 0.003086 \\ 0.003086 & 0.003086 \end{pmatrix} \begin{pmatrix} f6^{EQ} \checkmark \end{pmatrix} = \begin{pmatrix} 0.003086 & 0.003086 \\ 0.003086 & 0.003086 \end{pmatrix} \begin{pmatrix} f6^{EQ} \checkmark \end{pmatrix} = \begin{pmatrix} 0.00493827 & 0.0493827 \\ 0.0493827 & 0.0493827 \end{pmatrix}$$



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#### Bounce back collision









$$f(x+\xi\delta_t,\xi,t+\delta_t)-f(x,\xi,t)=-\frac{1}{\tau}\left[f(x,\xi,t)-f^{EQ}(x,\xi,t)\right]$$

$$\begin{aligned} \because \tau &= 1.0 \\ f(t + \delta t) - f &= -\frac{1}{\tau} \Big[ f - f^{EQ} \Big] \\ \Rightarrow f(t + \delta t) &= f - \Big[ f - f^{EQ} \Big] \\ \Rightarrow f(t + \delta t) &= f^{EQ} \end{aligned}$$

T=1.0 indicates that distribution function goes to equilibrium within the current time step



$$\begin{pmatrix} f1^{EQ} \rightarrow \end{pmatrix}' = \begin{pmatrix} 0.01234568 & 0.012345679 \\ 0.01234568 & 0.012345679 \end{pmatrix} \begin{pmatrix} f2^{EQ} \uparrow \end{pmatrix}' = \begin{pmatrix} 0.012345679 & 0.012345679 \\ 0.012345679 & 0.012345679 \end{pmatrix} \begin{pmatrix} f3^{EQ} \leftarrow \end{pmatrix}' = \begin{pmatrix} 0.01234567 & 0.012345679 \\ 0.01234567 & 0.012345679 \end{pmatrix} \begin{pmatrix} f4^{EQ} \downarrow \end{pmatrix}' = \begin{pmatrix} 0.012345679 & 0.012345679 \\ 0.012345679 & 0.012345679 \end{pmatrix} \begin{pmatrix} f5^{EQ} \searrow \end{pmatrix}' = \begin{pmatrix} 0.003086 & 0.003086 \\ 0.003086 & 0.003086 \end{pmatrix} \begin{pmatrix} f6^{EQ} \nearrow \end{pmatrix}' = \begin{pmatrix} 0.003086 & 0.003086 \\ 0.003086 & 0.003086 \end{pmatrix} \begin{pmatrix} f6^{EQ} \swarrow \end{pmatrix}' = \begin{pmatrix} 0.003086 & 0.003086 \\ 0.003086 & 0.003086 \end{pmatrix} \begin{pmatrix} f6^{EQ} \checkmark \end{pmatrix}' = \begin{pmatrix} 0.00493827 & 0.0493827 \\ 0.0493827 & 0.0493827 \end{pmatrix}$$



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#### Calculation results and visualization



#### **Problem Description**



Steady Fluid Flow through a channel with a block in the middle

 $\tau = 1.0$  $\rho = 1.0$ RT = 1/3

D2Q9 MODEL 11×11 mesh 100 active lattice

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#### MATLAB based calculation

#### Why?

- Every lattice contains a 9dimensional matrix
- Lengthy calculation hard to present by hand
- In MATLAB multi-dimensional matrix can be easily presented





#### MATLAB based calculation







# Numerical Example

Implementation and Results



#### Motivation

- Porous Media Flow
  - Discrete Simulation (NS) vs. Averaged Flow (Darcy)
  - Couple with transport/heat transfer
- Lattice-Boltzmann Methods
  - Incompressible Navier-Stokes
    - Water/Oil
  - Complex/Stochastic Geometries
    - Simple Meshing
  - Scalable
    - Large simulations







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1 8 5 5


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### Varying Grain Density (r = 2)



EGEE 520 Final Presentation

Presented By

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Varying Grain Size (5%)



Presented By



#### Non-Uniform Porosity





### Parallelism (Domain Decomposition)







#### Rock Sample Tomography





# Example Applications

Fancy stuff we can do with LBM



#### Examples

#### • Air Conditioner

- LBM simulates two conditions
  - 1. Fixed Fan Air Conditioner
  - 2. Sweeping Fan Air Conditioner
- Parallelism
  - Extremely High Resolution Simulation Required
  - Parallel computations allow LBM to be extremely efficient with reasonable computer hardware
  - Allowed for the billion grid points required to accurately simulate this case

#### http://youtu.be/I82uCa7SHSQ?t=21m20s



Image: https://www.youtube.com/watch?v=I82uCa7SHSQ





- Blood Clotting in a Human Artery
  - Arteries that have been affected by disease can be at high risk to rupture.
  - These ruptures can possibly be prevented by blood clotting in the vulnerable area
  - Need to simulate red blood cell changing from liquid to solid behavior and stick to artery wall.
    - LBM is effective at achieving this because of its hybrid particle/continuum nature



Image: https://www.youtube.com/watch?v=I82uCa7SHSQ





- Blood Clotting in a Human Artery
  - Parallelism
    - Using LBM, it is very easy to send different calculations to different processors
    - Allows for high efficiency when using computers with a high number of processors



Image: https://www.youtube.com/watch?v=I82uCa7SHSQ



#### Examples

- Turbulence Modeling
  - Models flow between two parallel plates
  - Large- eddy simulation approach
  - Replace Lattice Boltzmann equation with a filtered form
- Comparison to Spectral Method
  - Solution is virtually identical
  - LBM able to simulate with a 200x reduction in resolution
  - LBM much less computationally intensive in this case



Image: https://www.youtube.com/watch?v=I82uCa7SHSQ



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## Thank You!

Questions?