Direct Observation of Nanoscale Peltier and Joule Effects at Metal–Insulator Domain Walls in Vanadium Dioxide Nanobeams

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Supporting Information

ABSTRACT: The metal to insulator transition (MIT) of strongly correlated materials is subject to strong lattice coupling, which brings about the unique one-dimensional alignment of metal–insulator (M–I) domains along nanowires or nanobeams. Many studies have investigated the effects of stress on the MIT and hence the phase boundary, but few have directly examined the temperature profile across the metal–insulating interface. Here, we use thermoreflectance microscopy to create two-dimensional temperature maps of single-crystalline VO2 nanobeams under external bias in the phase coexisting regime. We directly observe highly localized alternating Peltier heating and cooling as well as Joule heating concentrated at the M–I domain boundaries, indicating the significance of the domain walls and band offsets. Utilizing the thermoreflectance technique, we are able to elucidate strain accumulation along the nanobeam and distinguish between two insulating phases of VO2 through detection of the opposite polarity of their respective thermoreflectance coefficients. Microelasticity theory was employed to predict favorable domain wall configurations, confirming the monoclinic phase identification.

KEYWORDS: Vanadium dioxide, thermoreflectance microscopy, Peltier effect, Joule heating, metal–insulator domain wall

Strongly correlated materials share a unique feature where phase transitions result in significant changes in physical properties, making these materials of particular interest for their potential device applications beyond the scope of current semiconductor technologies. Such devices are inherently complicated in nature owing to strong coupling of the crystal lattice with charge, spin, and orbital degrees of freedom of electrons. Vanadium dioxide (VO2) is one of such materials, extensively studied as it undergoes a highly stable high-temperature metal to low-temperature insulator transition (MIT) at T_{MIT, bulk} \approx 340 K.1 The electronic phase transition is accompanied by a structural transition in which a metallic rutile phase (M₉) converts to a semiconducting monoclinic phase (I),2 resulting in \sim 1% expansion of the lattice along the tetragonal c-axis (C₉).3,4 Multiple monoclinic lattice structures (I_{M1}, I_{M2}) are available for the insulating phase, which are almost optically identical and have very similar free energies,5 adding to the complexity of the material system. The more resistive I_{M2} phase has a lattice constant \sim 0.6% longer5 along C₉ than I_{M1} and can act as an intermediate state between I_{M1} and M₉, generally associated with higher tensile strains.6–10

One-dimensionally aligned metal–insulator (M–I) domain configurations can be attained either by substrate-induced uniaxial strain11–13 or nonuniform transition metal doping in a single-crystalline VO2 nanobeam (NB).14 In the former case, M₉ domains appear gradually upon heating, shifting T_{MIT} depending on the nature of external stress. Given a strong adhesive interaction with the substrate, I_{M1} phase (with longer lattice constant along C₉) becomes thermodynamically stable and the alternating M–I heterostructures are spontaneously organized (Figure 1a). This substrate-mediated MIT leads to a gradual decrease in electrical resistance until VO₂ NB becomes fully metallic around \sim 390 K (Figure 1b). Though it is generally believed that the MIT is induced by the symmetric splitting of the t₂g band composed of 3d vanadium states15 (Figure 1c), the physical nature of M–I wall is still undetermined and poorly understood despite its promising electrical and thermal applications at the nanometer scale.

In this letter, we investigate the electro-thermal activities at M–I walls by utilizing thermoreflectance imaging microscopy to create a thermal map of VO₂ NBs under current bias in the M–I coexisting phase regime. Thus far, electrical measurements

Received: January 5, 2014
Revised: April 7, 2014
Published: April 15, 2014
of the thermoelectric properties of VO₂ NBs have been conducted over the length of the device, determining effective material properties with indirect information about the domain interface. We report the direct observation of the highly localized Peltier cooling/heating and Joule heating at the M−I boundary, which acts as a thermal point source. In addition, our analysis suggests that an observed change in polarity of thermorelectance coefficient can differentiate between the IM1 and IM2 insulating phases while our calculation of the microelastic strain on the NB M−I interface establishes each monoclinic phase to have a unique and favorable domain wall configuration. These experiments provide insight into the native M−I heterostructures of VO₂ NBs. The M−I domain walls are expected to be truly nanometer-thick, suggesting exotic functionalities at the truly nanometer length scale.

The VO₂ NBs employed in this study were synthesized on 1 μm thick thermally grown SiO₂/Si substrates via a vapor transport approach. These single-crystalline NBs varied in length from 20 to 250 μm and typically had a 0.5 μm² rectangular cross-section. Optically clean NBs were preselected, and then devices were fabricated by conventional photolithography with two or four Au/Cr contacts deposited with 10 μm spacing using e-beam evaporation. Rapid thermal annealing at 525 K for 2 min was subsequently applied to achieve ohmic contact; negligible contact resistance was confirmed by a comparison of four-probe and two-probe I−V measurements. VO₂ NBs are naturally bonded to the SiO₂/Si substrate and experience uniaxial tensile strain along C_R (oriented as the NB long axis) as a result of high temperature growth and thermal expansion mismatch between the NB and the substrate.

We have visualized the thermal response of NB devices to electrical bias using charge-coupled device (CCD)-based thermorelectance thermal microscopy. This noninvasive method provides two-dimensional thermal images of a sample surface with 200−300 nm spatial and 10 mK temperature resolutions. The technique relies on the small but detectable variation of the surface reflectivity with temperature, as quantified by the thermorelectance coefficient C_TR, a material and illumination wavelength-dependent parameter that defines the relationship between the relative reflectivity change ΔR/R to the thermal field ΔT (relative to ambient) at the device surface: ΔT = (1/C_TR)(ΔR/R).

In the following experiments, we used a narrowband green LED (λ ≈ 530 nm) to illuminate the VO₂ NBs through a microscope objective with ×250 magnification and monitored the reflectivity of the NBs with a scientific grade CCD camera. Green illumination selected since the C_TR for the contact material (Au) is well-known at this wavelength. The thermal images presented in this letter assume a uniform C_TR of −2 × 10⁻⁴ K⁻¹. The NB substrate was mounted with a thin layer of...
thermal paste onto a Peltier heater for ambient temperature control. We then applied a 3.75 Hz sinusoidal voltage across (multiple) segments of the NB to create a slowly oscillating thermal field. The bias period was several orders of magnitude longer than the typical thermal response times of devices this size, ensuring that the NBs were operating in the quasi-static thermal regime. Bias current amplitudes were limited to $\sim 15 \mu A$ such that the NB domains were not displaced by electro-thermal effects in the $M^{-}-I$ coexisting state. We employed the minimum possible current bias that induced a measurable signal while remaining in the linear regime of the $I-V$ curve for the NB. We continuously monitored the optical image during the measurement to ensure the stable configuration of $M^{-}-I$ heterostructures along NBs.

The phase-locked CCD captured a periodic sequence of 8 images corresponding to eighth-period integrals of the reflectance signal under sinusoidal excitation. Data were averaged over $\sim 500$ periodic cycles to achieve sufficient signal-to-noise ratios. Adequate mathematical processing provided the magnitude and relative phase of the first and second harmonic components of the reflectivity field. This corresponds to a separation of the Peltier and Joule terms in the thermal field, given their respective linear (first harmonic) and quadratic (second harmonic) current dependencies. More detailed information regarding this technique including a

Figure 3. Thermal images of nonperiodic nanobeam (device 2) at 348 K under 8 $\mu A$ current excitation. Two NB segments and the adjoining electrode region are under current bias. (a−e) Initial thermoreflectance measurement images of device 2 before the RHS segment changed from $M^{-}-I-M$ to $M^{-}-I$ domain configuration. (f−j) Thermal images for the same current bias taken after the RHS segment stabilized. As domain walls are at substantial distances from each other, both Joule and Peltier phase images show heat exchange mainly with the substrate. Also note the change in the phase of the Joule heating in the RHS segment, which is an indication of different thermoreflectance coefficient for the two insulating phases.
diagram of the experimental setup may be found in the Supporting Information (see also refs 23 and 24).

Several NBs were examined in this manner, and it became apparent that each NB could be categorized into one of two observed trends depending on the strength of the attachment to the substrate (hence built-in strain): the first type exhibited periodic domain configuration and had a smooth decrease in resistance with temperature as described in Figure 1. The second type of NB displayed few and irregular domain formation, accompanied by a distinct jump in electrical resistance around $T_{MTT}$. For clarity, representative examples of each category, designated device 1 and device 2, respectively, are analyzed in this letter.

We first present results for a VO$_2$ NB (device 1), which exhibited the typical periodic domain configuration; Raman spectroscopy (Figure 1a) established this device was in the $M_1^{-1}M_2$ phase coexisting state. $^{10,25,26}$ Thermal images of the NB taken at 355 K under an applied 10 $\mu$A sinusoidal current are presented in Figure 2. As discussed, periodic domains are indicative of homogeneous substrate adhesion and are clearly observed in the optical image depicted in Figure 2a,b (greyscale image); this domain configuration remained stationary for the duration of the thermoreflectance measurement. Figure 2c,e displays the temperature magnitudes of the Peltier and Joule signals, respectively. Both signals originate in the interface regions between metal and insulator domains, which behave as thermal point sources. We expect to see Peltier heating or cooling at the $M_1$ junction given the presence of an energy barrier. $^{7,14}$ In this case, the signal may not be fully resolvable in an optical measurement due to the diffraction limit. However, Joule heating is also concentrated at the $M_1$ junction indicative of a significant resistance of the domain wall ($R_{DW}$) between the metallic and insulating domains. For the specific current amplitude depicted in these figures, Joule heating is stronger than the magnitude of Peltier and is consequently better resolved; the average ratio of the Joule magnitude to that of Peltier ($J/P$) is $\sim 1.75$. It is interesting to note that while $R_{DW}$ plays a minor role from an electrical standpoint (relative to the overall NB resistance), it is crucial from the perspective of the local thermal behavior of the NB. Thermal imaging reveals that the associated resistance is comprised in a very small region, leading to power densities at the $M_1$ junction that are much higher than that along the length of the NB. Highly localized Joule heating may also be attributed to the band offset between M and I domains through the possible introduction of an associated depletion region; however, the exact nature of the junction is still unknown.

Phase information from the thermal signal can be much more revealing as it is quite sensitive to small variations in the thermal distribution across the sample. The thermal response time of the NB is approximately 5 orders of magnitude shorter than the period of the applied current, leading to uniform thermal phase. Thus, any deviations in the phase image are due to bipolar behavior (cooling instead of heating) or sign changes in the $C_{TR}$. The Peltier phase image (Figure 2d) depicts both heating and cooling localized at the $M_1$ interfaces: when one interface is heating (under forward bias), the neighboring interface is clearly cooling (under reverse bias) denoted by the 180° phase shift. As expected, the Joule signal (Figure 2f) does not exhibit this phase shift and is always heating.

While the Peltier signal is seemingly concentrated inside the insulating region, we expect the actual thermal activity to also present in the metal region. We attribute the apparent lack of thermal signal over the metallic state to a small thermoreflectance coefficient, as the images are based on a uniform $C_{TR}$ calibrated for Au only. Phase-shifted Joule activity is evident in the metal regions of the NB and into the substrate owing to its stronger signal but is not visible in the magnitude images. To explain this result, the $C_{TR}$ of the metal phase must be of opposite sign and significantly smaller in magnitude than that of the insulating state. It is evident in Figure 2f that the supporting substrate of the sample also functions as a heat sink for Joule heating. The signal spreads outward uniformly from its peak at the domain walls, demonstrating good thermal contact between the NB and the substrate. The lack of Peltier substrate activity is not simply because of its lesser signal magnitude. Heating and cooling signals at nearby domain walls are mainly coupled through the nanobeam with little leakage into the substrate; this interaction may diminish the overall Peltier magnitude in this device. Through inspection of the phase images, we can confirm that the resultant reflectivity signals are due to thermal fluctuations and not movement at the domain boundaries. The uniform thermal signals at the interfaces occur over a larger width than expected for edge effects from movement not observed optically. In addition, the point source-like behavior with continuous activity into other regions of the image (nearby substrate) would not be possible.

The apparent total strain (and thus domain pattern) differed between samples due to nonuniform substrate adhesion, variations in growth temperature, and stress induced by the end-to-end clamping by the contacts. In this sense, NBs with a nonperiodic M–I domain pattern are possible and display quite different temperature-dependent behavior, as is shown in Figure 3 for a sample (device 2) held at 348 K. Current was applied across two consecutive segments of the NB (Figure 3a,f); referred to in this letter as the right-hand side (RHS) segment and the left-hand side (LHS) segment. Irregular domain patterns nucleated from the side contacts at 328 K, a much lower ambient temperature as compared to device 1 and considering $T_{MTT,Bulk}$. The domain walls in both segments were initially at a $\sim 50^\circ$ angle relative to the NB long axis. The domain configuration and angled domain walls of this NB can be indicative of nonuniform stress distribution along the length and width of the NB, $^{8,12,13}$ suggesting weak substrate interaction and/or clamping strain from the Au contacts.

For the thermoreflectance measurement, we applied sinusoidal current at varying amplitudes, ranging from 5 to 10 $\mu$A, very similar in magnitude to the previous NB as this was the minimum necessary to resolve the Peltier signal. After one measurement run at 8 $\mu$A bias, the domain configuration on the RHS changed from M–I–M with angled domain walls (Figure 3a–e) to M–I with a single vertical wall (Figure 3f–j), possibly due to excessive Joule heating at the interface. The new domain configuration was stable for all subsequent measurements.

The magnitude of Peltier temperature in the RHS segment was very similar to that of uniformly clamped NB (Figure 2c); however, Joule heating was substantially greater. For the same current bias applied for device 1 (10 $\mu$A), $J/P_{bias} \approx 7$ and $J/P_{LHS} \approx 5$. Such significant Joule heating, especially on the RHS, could drive the domains to another insulating state (from $I_{MT}$ to $I_{LHS}$). These highly localized junction Peltier and Joule effects are also responsible for M–I domain wall propagation along the VO$_2$ NBs at high currents (well above those used during the measurement), as previously reported in suspended W$_x$V$_{1-x}$O$_2$ NBs. $^{2}$ This is especially true for device 2, as the NB does not dissipate Joule heating well into the substrate possibly due to
weaker adhesion. The resultant phase oscillation could be controlled and sustained with the addition of a parallel capacitor by repeating the charging and discharging process (see Supporting Information).

The phase images of both Peltier (Figure 3c,h) and Joule (Figure 3e,j) confirm the earlier premise that the signals occur at the domain walls. The typical spreading pattern from a thermal point source is detected along the NB and into the substrate. The relative signal strengths along the NB show heat diffuses preferentially in the metal region of the RHS segment, possibly owing to its higher thermal conductivity. Activity along the Au-covered-NB region gives us a reference value for $C_{TR}$ as this is known to be negative for Au at this illumination wavelength. From this and the expected uniformity of the Joule phase activity, we gain valuable insight about $C_{TR}$ of the other regions. $C_{TR}$ of the metal domains is always positive, while the $C_{TR}$ of the insulator domain on the RHS segment of measurement 2 is negative (Figure 3j, RHS), similar to the scenario presented for device 1 in Figure 2. However, the insulating state in the LHS segment during the same measurement is roughly 180° out of phase from the aforementioned insulator domains, implying a positive $C_{TR}$ (Figure 3j, LHS). We believe that the difference in the sign of $C_{TR}$ between these two insulating domains distinguishes the two monoclinic phases of VO$_2$; that is, the reflectivity dependence on temperature variations has the opposite behavior for the two monoclinic states. This is in agreement with the phase information for the RHS segment before the change to the single vertical domain wall; the insulator domain on the RHS during measurement 1 (Figure 3e) is roughly 180° phase shifted from the I domain in the RHS during measurement 2 (Figure 3j) for the same excitation bias. For clarity, the average phase values of the NB regions associated with this analysis are presented below the phase images in Figure 3e,j. The significant change in the thermorelectance properties between the two insulating phases could be attributed to the difference in reflective signatures of the two monoclinic phases under polarized light.$^{6,26,29}$ Further thermorelectance measurements using a polarized light source would illuminate the underlying mechanism of the $C_{TR}$ sign change.

We applied Khachaturyan’s microelasticity theory for a single coherent inclusion in the matrix of a parent phase$^{30}$ to analyze the elastic energy and thus orientation of the M–I interface of a VO$_2$ NB in an attempt to understand the change in domain wall alignment. Both the $M_R/I_M$ and $M_R/I_M$ junctions are considered coherent. As shown in our previous work,$^{31}$ both rutile–monoclinic structural transitions have four possible variants each with different stress-free transformation strains, leading to eight possible domain wall configurations all with minimized elastic energy density. The favored orientation exhibits reduced total elastic energy, which is related to the geometry of NB; accordingly, $M_R/I_M$ will favor an acute angle of 56° (Figure 4) with the NB top surface, while $M_R/I_M$ may display an 89° (Figure 4) or 33° acute angle. This is consistent with the experimentally observed angles of devices 1 and 2 whose insulating states are identified through the sign of $C_{TR}$ during thermorelectance imaging: the $M_R/I_M$ domain wall exhibits an angle of 48–52° and $M_R/I_M$ presents as a 90° interface (Figures 2 and 3). More details on the calculation of domain wall configurations can be found in the Supporting Information.

Further evidence identifying the insulating phases of device 1 and 2 is obtained by examining the resistance trend with ambient temperature of the two NBs (Figure 5). Device 2 exhibits a large jump in resistance at 335 K, coinciding with the appearance of the first metal domain. This implies that either $R_{WV}$ is quite large, ~300 kΩ, or that $I_M$ converted to the more resistive $I_M$ insulating state, similar to the behavior described in Kasirga et al.$^{9}$ In contrast, device 1 shows a fairly steady decrease in resistance before becoming fully metallic. Both NBs
display the expected Arrhenius behavior for a nondegenerately doped semiconductor before the metal domains emerge, $R_f(T) = R_0 e^{E_f/k_BT}$. However, device 2 has a markedly lower overall resistance despite similar sample geometries; thus, the two NBs have quite dissimilar activation energy: $E_{a(dev1)} ≈ 0.3$ eV and $E_{a(dev2)} ≈ 0.11$ eV; both are consistent with values reported in the literature ranging from 0.08 to 0.36 eV.27,29,32,33 The lower activation energy suggests device 2 to be more highly doped.

The irregular domain patterns composed of four factors:

$$R_f(T) = x(T)R_f(T) + [1 - x(T)]R_M(T) + R_C + R_{DW}$$

where $x(T)$ is the length fraction of the NB in the I state at a given ambient temperature, and $R_f$ and $R_M$ are the expected insulating and metal resistances, respectively. The contact resistance, $R_C$, was shown to be negligible. We used this equation and the extrapolated Arrhenius fitting at multiple ambient temperatures to determine $R_{DW}$ of the more uniform NB (device 1), which we found to be $39 ± 7$ kΩ. This value is in agreement with the figure put forth in Wei et al.\textsuperscript{32}

The jump in resistance, sign change of the $C_{TR}$, and transformation of the interface angle of device 2 denote the change in monoclinic crystal structure in the M–I coexisting state. $T_{MIT-dev2}$ is a lower temperature than $T_{MIT-Bulk}$ indicating compressive strain driving the NB to the phases with smaller lattice constants (M$_B$ and I$_M$). The irregular domain patterns in addition to strong Joule activity at the M–I interface suggest poor substrate bonding, which would reduce tensile stress felt by the NB upon cooling from the high growth temperature ($-1000$ °C). Thus, device 2 was initially in the I$_M$ state. At elevated temperatures, the appearance of metal domains alleviates compressive strain while inducing tensile strain in the adjacent insulating domain. The induced strain, accompanied by intense Joule heating in the RHS segment generated by the current applied during the measurement, stimulated the conversion from I$_M$ phase to I$_{M2}$.

VO$_2$ NBs with good substrate adhesion would experience tensile strain at the temperatures of this experiment. Homogenous periodicity and uniform thermal signal in the substrate demonstrate uniaxial tensile strain in device 1 along the NB long axis, fixing the insulating phase to the I$_{M2}$ phase with a longer lattice constant. The higher overall resistance and the persistence of I domains with vertical interfaces to 390 K, accompanied by intense Joule heating in the RHS segment generated by the current applied during the measurement, stimulated the conversion from I$_{M2}$ phase to I$_{M2}$.

In conclusion, our results directly reveal the extremely local Peltier and Joule effects across the M–I domain walls. Thermal images show that alternating Peltier heating and cooling at neighboring domain interfaces exchange energy through the nanobeam; while Joule heating dissipates in the substrate. We show that significant domain wall resistance is responsible for concentrated Joule heating. The insight gained through thermoreflectance imaging and the ability to distinguish between insulating phases illuminate the underlying impact of stress on the nanobeam, while examination of the elastic energy at the interface determines the favored wall configurations to minimize the total elastic strain for each monoclinic phase.

## ASSOCIATED CONTENT

### Supporting Information

Detailed methods and figures describe thermoreflectance microscopy technique. Supporting Information regarding the theoretical calculation of the elastic energy and domain wall oscillation at high applied currents are also provided. This material is available free of charge via the Internet at http://pubs.acs.org.

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### Notes

The authors declare no competing financial interest.

## ACKNOWLEDGMENTS

The work at UC Berkeley was supported by the US Department of Energy Early Career Award under the Award No. DE-FG02-11ER46796. The work at Penn State was supported by the National Science Foundation through grants DMR-0820404, DMR-1006541, and DMR-1210588. The work at UCSC/Purdue was supported by the Center for Energy Efficient Materials, an Energy Frontier Research Center funded by the U.S. Department of Energy, Office of Basic Energy Sciences under Award Number DE-SC0001009.

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