USE OF CARBON FOR REMOVAL OF AMMONIA FROM WATER^{*} O. P. Mahajan, A. Youssef and P. L. Walker, Jr. Department of Material Sciences The Pennsylvania State University University Park, PA 16802

Introduction

Ammonia is produced in waste water and sewage treatment plants. The presence of ammonia in water is undesirable because ultimately it gets converted into nitrites and nitrates which act as nutrients for algae growth. The present study describes the use of surface-modified carbons for the removal of ammonia.

Experimental

Activated carbons supplied by five different companies, namely A (12x40 mesh), B (4x10 mesh), C (8x30 mesh), D (6x8 mesh) and E (4x10 mesh) were used. These carbons had N₂ areas (77°K) in the range 750-830 m²/g and CO₂ areas² (298°K) in the range 540-825 m²/g. Aqueous suspensions of the carbons had alkaline pH values in the range 7.1-9.1.

The as-received carbons were given oxidative treatments with dry and moist air at 285°C, HNO₃, 0.2N $(NH_4)_2S_2O_8$ (ammonium persulfate), and 2N H₂O₂. Moist air refers to an air-water vapor mixture at a total pressure of 1 atm containing water vapor at a partial pressure of 17 Torr. For treatment with HNO₃, carbon was heated with concentrated HNO₃ (10 cm³ HNO₃/g carbon) to dryness at 80°C. For treatment with $(NH_4)_2S_2O_8$ and H_2O_2 , 2g portions were mixed with 50 cm³ of the oxidizing solution. The suspensions were shaken mechanically for 48 hr at room temperature. After oxidative treatment with different oxidizing solutions, the carbons were washed free of excess oxidants with water and dried at 110°C.

Neutralization of 0.1N solutions of NaOH, NaH-CO₃, Na₂CO₃ and NH₄OH by carbons was determined by mixing Ig portions with 100 cm³ of solution. After attainment of equilibrium, the fall in concentration of NaOH, NaHCO₃ and Na₂CO₃ solutions was determined by titration with HCl, whereas decrease in concentration of ammonia was determined using an Orion ammonia electrode.

The efficacy of carbons for removal of ammonia under dynamic (flow) conditions was studied in a Pyrex glass column of 2 in diameter. The carbon bed (height, 4 in) was held between two glass wool plugs (height, 2 in). During the runs, the level of ammonia in the column was always kept constant (about 2 in above the upper glass wool plug). Ammonia was passed through the bed at a constant flow rate. The concentration of ammonia in the effluent was followed as a function of time until the outlet concentration equalled the inlet concentration. The 'spent' carbon was regenerated with 0.1N HCl followed by washing with water until free from chloride ions.

Results and Discussion

The as-received carbons did not adsorb noticeable amounts of ammonia. However, following oxidation all the carbons adsorb significant amounts of *Supported by the Office of Water Research and Technology.

ammonia (Table 1). The pH values of aqueous suspensions of various oxidized samples and the amounts of various bases neutralized by the carbons are listed in Table 1. The efficiency of various oxidative treatments to enhance ammonia uptake of a given carbon follows the order: $HNO_3 > (NH_4)_2S_2O_8 > H_2O_2 > moist$ air > dry air. Amounts of NaHCO₃, Na₂CO₃ and NaOH neutralized by various samples follow the same trend as the adsorption of ammonia, whereas pH values of the aqueous suspensions decrease in the reverse order. For a given carbon, the amounts of different bases neutralized vary in the order

$$NaOH > Na_2CO_3 > NH_0H > NaHCO_3$$

Various oxidative treatments had little or no effect on surface areas of carbons. Although for each oxidative treatment surface areas of samples derived from carbon C are lower than those of the other carbons, samples from carbon C have the highest ammonia removal capacities. The high surface area of activated carbon often determines its use in most industrial applications. However, in the present study the chemical nature of the surface, rather than the magnitude of the surface, determines ammonia removal capacity.

Boehm (1) has suggested a selective neutralization technique using NaHCO₃, Na₂CO₃ and NaOH for estimating the concentration of carboxylic, lactonic and phenolic acid groups. He has concluded that NaHCO₃ neutralizes carboxylic groups, Na₂CO₃ neutralizes carboxylic and lactonic groups, and NaOH neutralizes carboxylic, lactonic and phenolic groups. That is, NaOH gives a measure of total surface acidity of carbons. Boehm also found that for completely oxidized carbons twice as many acid groups were neutralized with Na₂CO₃ as with NaHCO₃, whereas with NaOH three times the NaHCO₃ neutralization was achieved.

In the present study when the amounts of NaHCO₃, Na₂CO₃ and NH₄OH neutralized by different samples were plotted against amounts of NaOH neutralized, the data points in each case fell more or less on straight lines passing through the origin. From the plots, ratios of NaHCO₃, NH₄OH and Na₂CO₃ neutralized relative to NaOH were found to be 0.36, 0.51 and 0.63, respectively. These results show that for a given carbon, irrespective of the organic precursor, amount and nature of inorganic impurities present, the activation process, the degree of activation and subsequent oxidative treatment, the concentration of acid groups of different strengths relative to the total surface acidity is more or less constant.

Since the amount of Na $_2$ CO $_3$ neutralized by a carbon has been suggested to be a measure of the concentration of carboxyl and lactone groups (1), the amount of CO $_2$ evolved on outgassing a carbon at elevated temperatures should be theoretically equivalent to the Na $_2$ CO $_3$ neutralization capacity.

However, in this study amounts of ${\rm CO}_2$ evolved were invariably greater than the ${\rm Na}_2{\rm CO}_3$ values.

Carbons A and C oxidized with HNO₃ were used in dynamic studies. Breakthrough times and bed capacities for different flow rates are listed in Table 2. Breakthrough times increase with decreasing flow rates, as expected. Capacities are independent of flow rate after the first cycle, indicating the presence of minimal external mass transport resistance to adsorption. Regeneration of the carbon beds between successive runs was conducted by treatment with HC1. Following the first ammonia adsorption run, about 95% of the ammonia adsorbed could be 'desorbed' with HC1. In subsequent runs, essentially all adsorbed ammonia could be desorbed. The irreversibly adsorbed ammonia has been suggested to be due to the presence of some, as yet unidentified, surface functional group (2).

In conclusion, the results of the present study suggest that oxidized carbons, preferably those oxidized with HNO₃, should be strong contenders for ammonia removal from waste waters.

References

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Table 1 - BASE NEUTRALIZATION CAPACITIES AND pH VALUES OF CARBONS

Oxidizing			<u>Base</u> neu	tralizati	on capacit	y, m-equiv/g
Agent	Carbon	рН	NaHCO3	NH40H	Na_2CO_3	NaOH
HNO ₃	Α	4.40	1.40	1.80	2.30	3.60
	В	4.40	1.25	1.60	2.10	3.20
	С	4.02	2.15	2.80	3.55	5.55
	D	4.35	1.30	1.70	2.20	3.60
	Е	4.35	1.35	1.80	2.25	3.65
(NH ₄) ₂ S ₂ O ₈	А	4.95	0.95	1.40	1.70	2.65
	В	4.95	0.90	1.40	1.70	2.65
	С	4.14	1.70	2.60	3.25	4.95
	D	4.92	1.65	1.60	1.95	3.00
	Е	4.82	0.95	1.40	1.75	2.65
^H 2 ⁰ 2	Α	5.25	0.60	0.90	1.05	1.60
	в	5.30	0.65	0.90	1.05	1.65
	С	4.28	0.80	1.20	1.40	2.20
	D	5.22	0.45	0.70	0.80	1.25
	Е	5.11	0.60	0.90	1.05	1.65
Moist air	Α	5.60	0.40	0.65	0.65	1.05
	В	5.27	0.40	0.65	0.70	1.15
	С	5.14	0.55	0.85	0.85	1.40
	D	5.28	0.40	0.65	0.60	1.00
	E	5.65	0.45	0.85	0.75	1.20
Dry air	Α	5.81	0.20	0.40	0.45	0.70
	В	5.31	0.20	0.40	0.45	0.65
	С	5.15	0.35	0.70	0.85	1.25
	D	5.30	0.20	0.40	0.45	0.65
	E	5.65	0.32	0.60	0.75	1.10

Table 2 - BREAKTHROUGH TIMES AND BED CAPACITIES

Sample	Flow rate (cm ³ /min)	Breakthrough time (min)	Bed capacity (m-equiv/g)
	95	30	2.63
С	95	30	2.48
	125	22	2.46
	165	16	2.46
	200	13	2.44
	280	10	2.42
A	90	20	1.68
	90	20	1.58
	130	14	1.59
	165	11	1.56
	200	9	1.56
	260	7	1.52