

4.3 Surfactant Soil Washing

- Mechanisms:
1. Micellar solubilization of hydrophobic hydrocarbons.
 2. Conversion into an emulsion
 3. Reduce surface tension $\rightarrow \uparrow$ mobility
 4. Coalescence of ganglia into single bank
- \therefore similar to cosolvents and alkalis.

Two regions of interfacial tensions:

1. Low surfactant conc. (1-2 wt%) two-phase system (oil/water)
2. High surfactant conc. (2-10 wt%) three-phase with micro-emulsion in equilibrium with (oil/water)

The emulsion will preferentially separate to the water or oil phase depending on:

1. Salinity: ✓ 1% NaCl conc \rightarrow water
✗ 3% NaCl conc \rightarrow oil
 2. Surfactant solution conc. (low conc = water)
 3. Temperature ✓ High temp \rightarrow water
- } Best to have mono-emulsion between oil-water since low T and removable under reasonable hydraulic gradients.

Field Implementation

↓ Continuous low conc. (<1% wt) - continuous flush (^{multiple p.v.})

Two strategies: (1) Solubility enhanced or (2) Displacement process

Keep M<1. Use conc. solution 10-40 wt% as finite slug.

Injection and production wells.

Sometimes horizontal.

Heterogeneities may affect results.

Level of Demonstration

Several decontaminations:

Volk Nat. Guard Base (WI) TCA, TCE to 3 - 300 ppm

Sandy soils with $K = 0.015 \text{ m/d}$

$$K = 10^{-4} - 10^{-2} \text{ cm/s}$$

Lab tests $\rightarrow 74\% - 94\%$ NAPL recovery in 12 pore volumes.

Field - @ 14 pore vols. 3 test holes g/c clogged by 3rd day.

Laramie, Wyoming

Creosotes. Isolation cell of pore volume 5000 gal.

Injection of 30,000 gal surfactant } recovered - 260 gal
149,000 gal waterflood } - 1600 gal
 $\sim 95\%$ concentration reduced.

Borden (1990) $K = 10^{-4} \text{ m/s}$ 3x3m cell.

231 l. PCB released - migration for 2 months

48 l \rightarrow pumping

52 l \rightarrow excavation of upper 1m.

Backfilled with bentonite cap

12 l \rightarrow Waterflood

62 l \rightarrow 14.4 pore volumes of surfactant ($1 \text{ PV} = 2400 \text{ gal}$)
over 4 months

10 l \rightarrow Soil samples reveal less than 10 l left.

182 l of 231 l

$\sim 50 \text{ l}$ missing

perhaps volatilization, @ sheetpile porosity,
or \downarrow migration in fractures caused
by sheet piling.

Also used for PCBs
Carbon Tet.

Applicability/Limitations

Applicable to most DNAPL sites.

Toxicity and recovery of surfactant are key.

↓ or may cause downward migration

Recovery strongly affected by heterogeneities

1. Sweep process (conc. > 10%) for high DNAPL concentration at sites
2. Solubilization (conc. ~1%) for low concentration of DNAPL this controls fugitive DNAPL migration

Cost and Availability

Hardware available

Full scale application in cont. areas completed.

Potential use with co-solvents.

No case information.

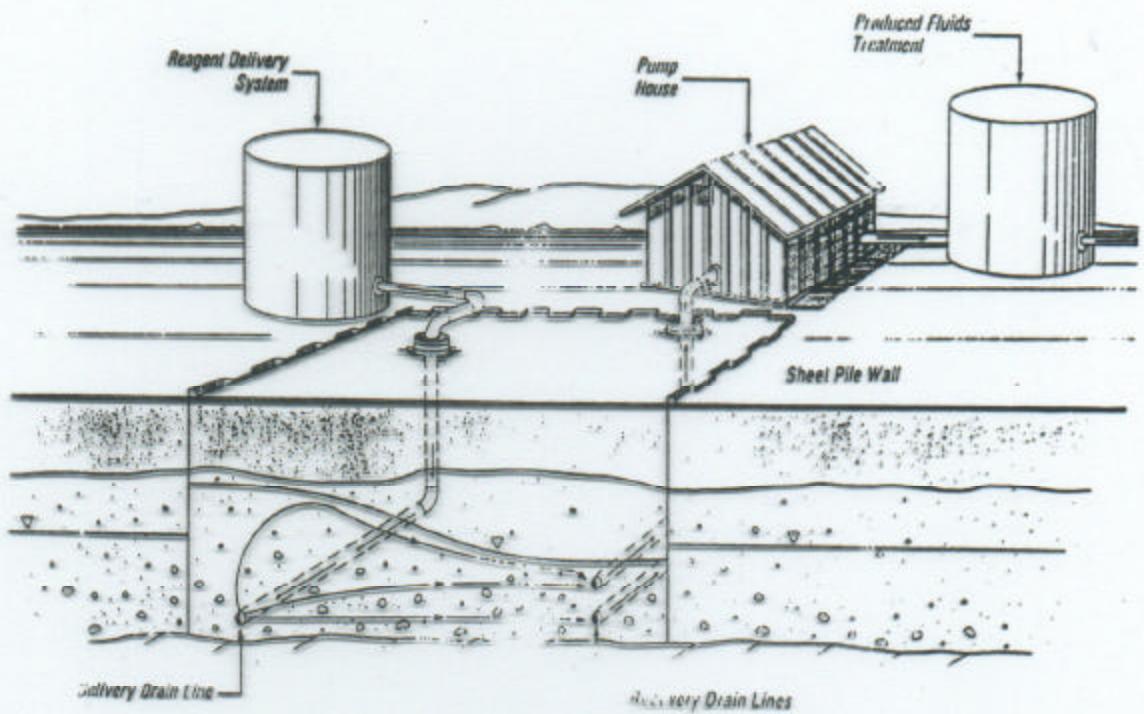


Figure 3.5.3.5 Schematic of dual drain line system for the 1988 field test using water and combined alkali/surfactant flooding of heavy oils [Sale et al., 1989].

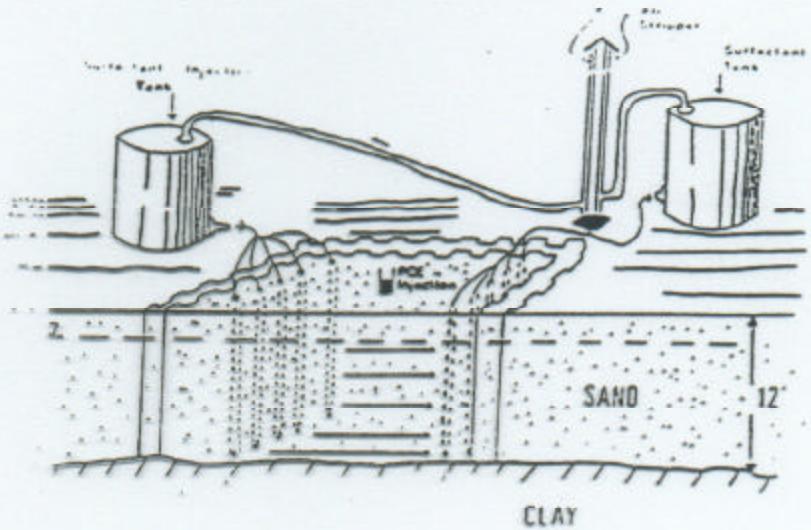


Figure 3.5.3.6 Schematic of field test using water and surfactant flooding for enhanced PCE recovery (Borden, Canada) [Fountain et al., 1990].