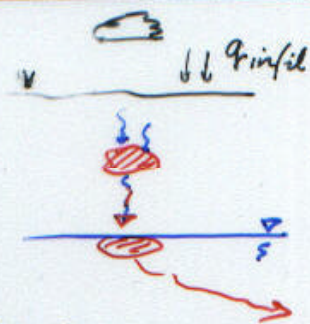


7.1.2 ADVECTION DUE TO INFILTRATION



① Assume steady vertical plug flow displacement

$$v_w^a = \frac{q_{infil}}{\theta_w}$$

q_{infil} = Infiltration amount

v_w^a = Advective velocity of water

θ_w = Volumetric moisture content

Resulting infiltration - advective flux

$$q_M = \underbrace{\theta_w v_w^a}_{\text{Darcy flux (velocity)}} c_w$$

q_w = Darcy volumetric flux.

q_M = mass flux.

Note: c_w max is solubility (aqueous).

Conservation of mass \Rightarrow Gaseous and Aqueous Transport

(Aqueous is carried by infiltration)

i.e. Net reduction of source volume by:

- Gaseous diffusion:
- Aqueous movement:

$$R \frac{\partial c_g}{\partial t} = D_g^* \frac{\partial^2 c_g}{\partial x^2} - \underbrace{\frac{\theta_w}{\theta_g} \cdot \frac{1}{H}}_{\text{Partitioning of vapor into water}} v_w^a \frac{\partial c_g}{\partial x}$$

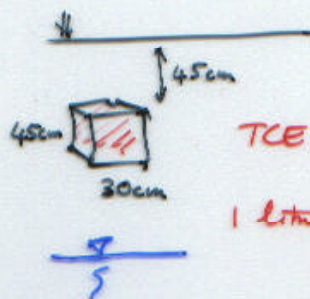
Partitioning of vapor into water
- same as in R.

Neglects:

- Aqueous dispersion
- ~~A~~ Gaseous advection.

Estimates of aqueous transport

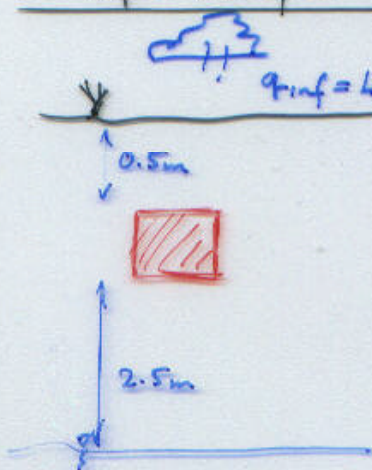
eg. Border TCE experiment



TCE @ residual sat.

1 litre of TCE over
45 x 30 cm area
~ 16 L/m²

No vapor transport (assume)



$q_{inf} = 45 \text{ cm/yr}$

$\theta_w = 10\%$

Solubility, $S \equiv C_w = 1100 \text{ mg/L}$

Questions?:

① How long to reach water table:

$$v_w^a = \frac{q_{inf}}{\theta_w} = \frac{.45 \text{ m/yr}}{.1} = 4.5 \text{ m/yr}$$

$\therefore 2.5 \text{ m travel} \approx \frac{1}{2} \text{ year}$

(This ignores retardation).

② What loading from aqueous phase (i.e. q_M)

$$q_M = \theta_w v_w^a C_w = (0.1)(4.5)(1100 \text{ mg/L})$$

Note: $1 \text{ m/yr} \equiv 1 (\text{m}^3/\text{yr}) \text{ per m}^2$

$$q_M = 0.45 \text{ m/yr} (1100 \text{ mg/L})$$

$$\begin{aligned} .45 \text{ m}^3 &= 450 \text{ L} \quad \therefore q_M = 450 \text{ L} \times 1100 \text{ mg/L} \\ &\approx .5 \times 10^6 \text{ mg} \\ &\approx \underline{\underline{.5 \text{ Kg/yr. per m}^2}} \end{aligned}$$

Relatively small loading - removed from source.

LOADINGS MAY BE CHECKED USING MORE SOPHISTICATED MODEL

Transport Examples

porous medium:

$$\theta_w = 10\%$$

$$\theta_s = 25\%$$

$$q_{inf} = 45 \text{ cm/yr}$$

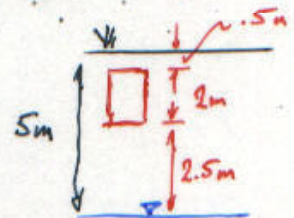
depth to watertable 5 m

$$f_{oc} = 0.01\%$$

$$\rho_b = 1.65 \text{ g/cm}^3$$

very low sorption onto organic

$$q_{inf} = 0.65 \text{ m}$$



TCE @ 20°C:

$$D_s = 8.1 \times 10^{-6} \text{ m}^2/\text{sec} \quad \text{Gaseous diffusion coef.}$$

$$H = 0.30$$

$$K_{oc} = 126 \text{ ml/g}$$

$$P_v = 60 \text{ mm Hg} \quad (C_s = 7.9\%)$$

$$S = 1100 \text{ mg/l}$$

source:

height 2.0 m

radius 1.0 m

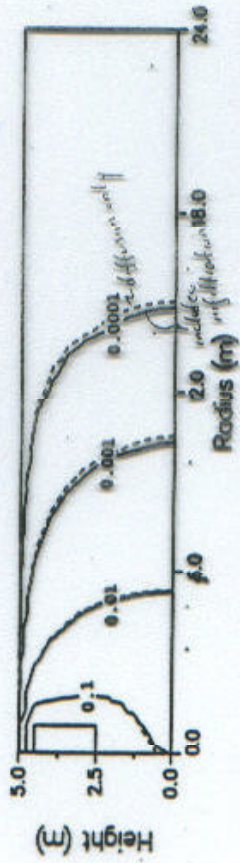
depth to top 0.5 m

Gaseous and Aqueous Transport

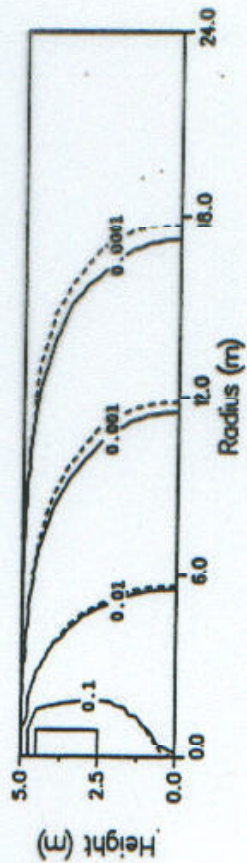
Example

- **uncovered ground surface**

- *Passive remediation (good)*
- *Infiltration to groundwater (bad)*



5.75 kg to groundwater after 6 months



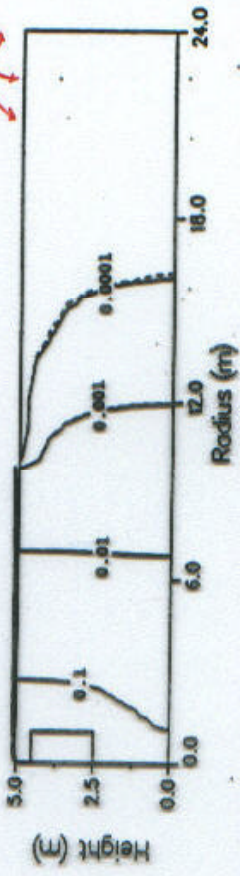
15.8 kg to groundwater after 1 year

Gaseous and Aqueous Transport

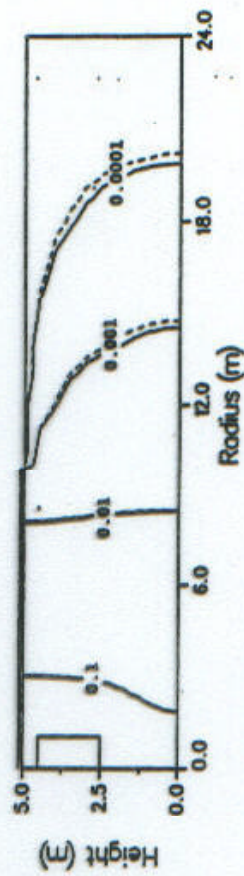
Example

- **covered ground surface** ∴ *No infiltration*

- *Decreased passive remediation (bad?)*
- *Decreased infiltration (good)*



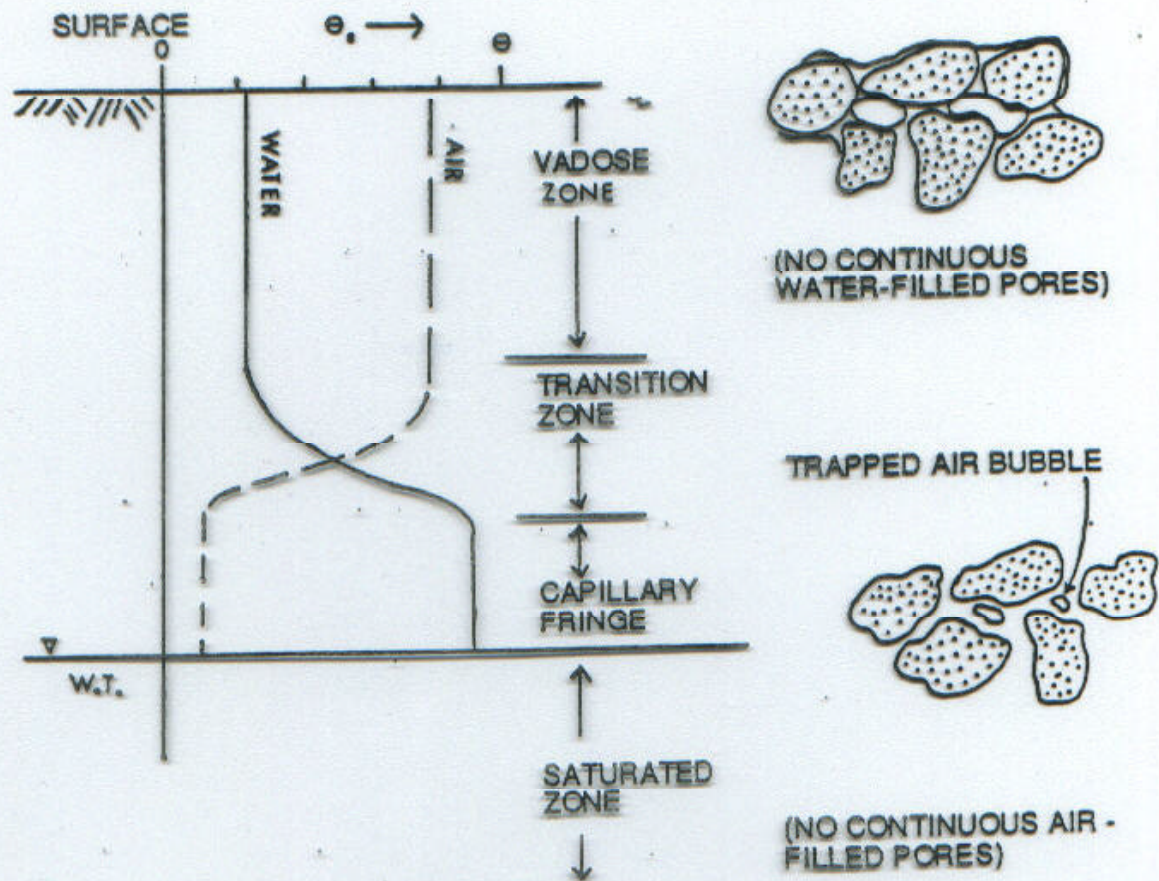
0.35 kg to groundwater after 6 months



2.95 kg to groundwater after 1 year

A = INFILTRATION

Watertable (Capillary Fringe) Boundary

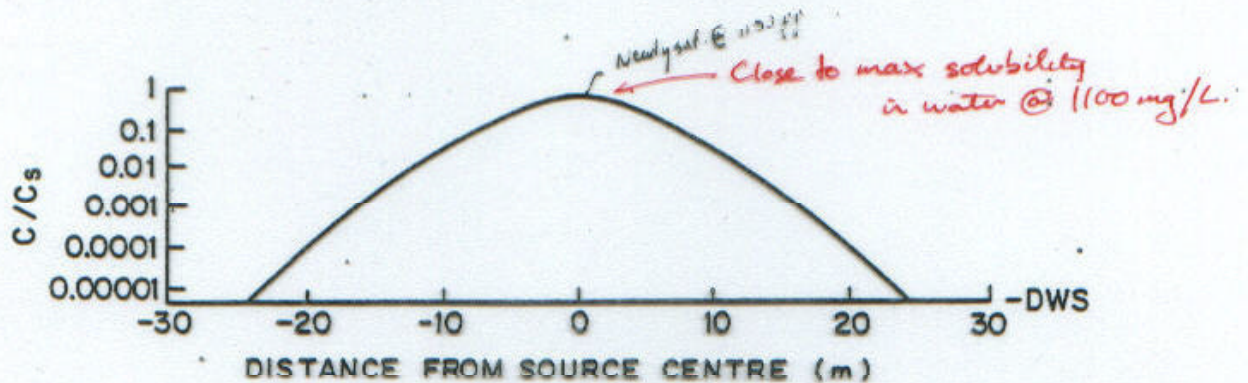


- very slow vapour transport in transition zone
 - top of fringe impermeable to vapours
- but, contaminants partition to water

Watertable Fluctuation

- contaminated soil moisture placed in saturated zone
- consider diffusive transport example

watertable concentration profile
(covered; after 6 months)



- a 50 cm rise in watertable elevation

→ 3.3 kg TCE placed in groundwater

*This is an order of magnitude increase
in water table loading - from 0.35 kg.*